

ELECTRONICS Lecture for PSI Course

①

A. Schöning, August 2013

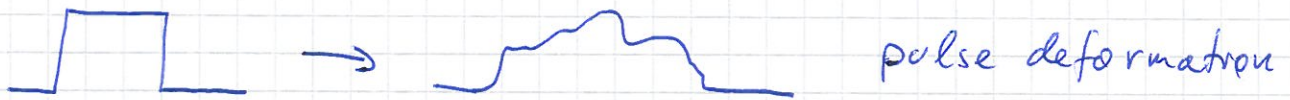
Overview

- Pulse terminology
- Cables and signal transmissions
- Noise + filters
- Components analog/digital
- Signal Standards

BOOK: W. R. LEO

Techniques for Nuclear and
Particle Physics Exp.

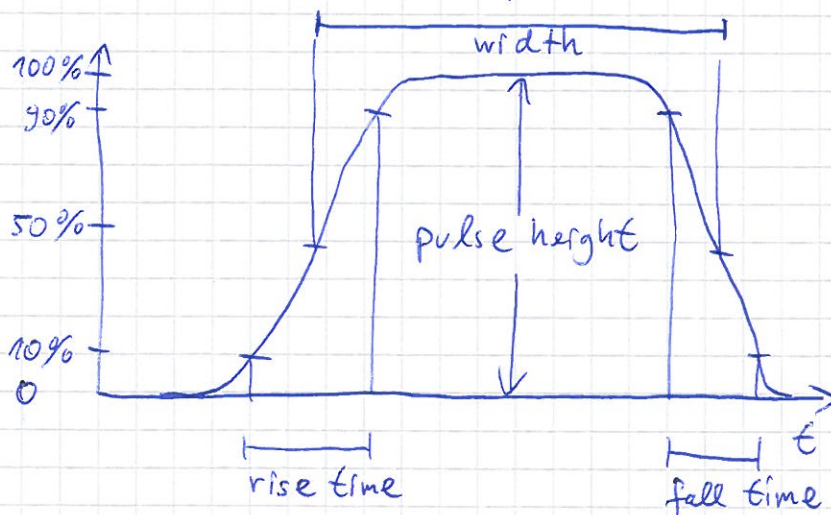
Transmission of Signals



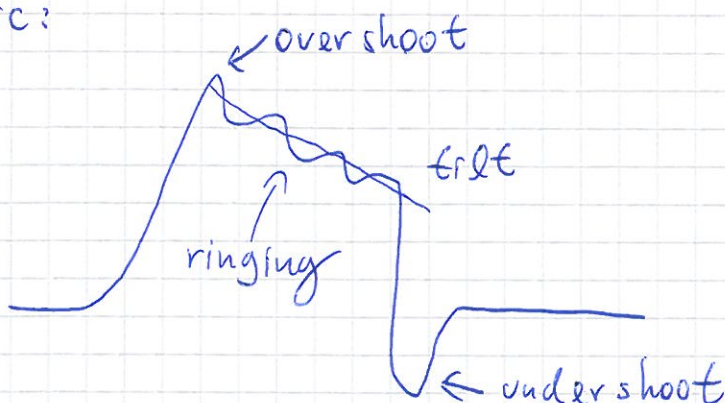
depends on:

- resistance (power consumption)
- noise (capacities, inductance)
- signal quality (deformation, attenuation)
- signal transmission speed
- digital / analog
- bandwidth (frequency behaviour)

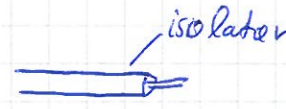


Pulse Terminology



realistic:

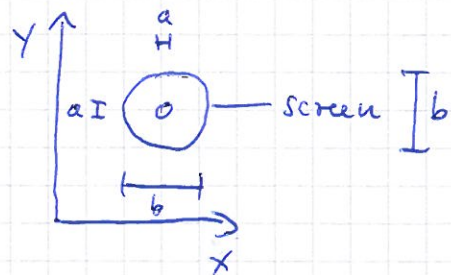
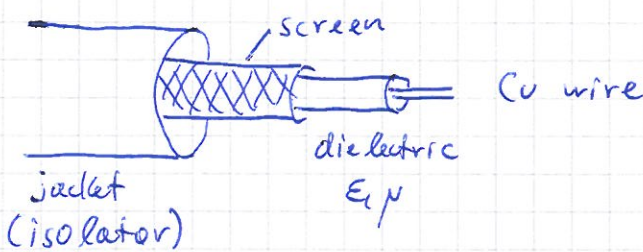


0 Cable Types

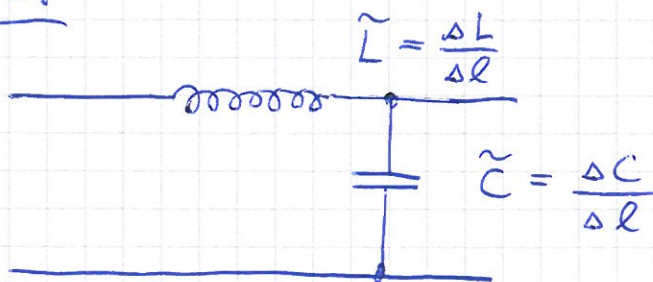
- 1 wire/cord (Litze) 
- 2 flat ribbon 
- 3 twisted pair  $Q = Q_+ - Q_-$
- 4 coax

1, 2, 3 \Rightarrow large signal deformation
 - only short distances
 - only low frequencies ($\leq 1 \text{ MHz}$)

Coax Cable



Circuit:



$\tilde{L}, \tilde{C} > 0$ leads to losses
 - dielectric losses
 - skin effect

every cable has a capacity and inductance!

$$\tilde{C} = \frac{\Delta C}{\Delta l} = \frac{2\pi \epsilon}{\ln(b/a)} = \frac{\epsilon_r \cdot 55.6 \text{ pF/m}}{\ln(b/a)}$$

$\epsilon_r = 2.3$ for PE

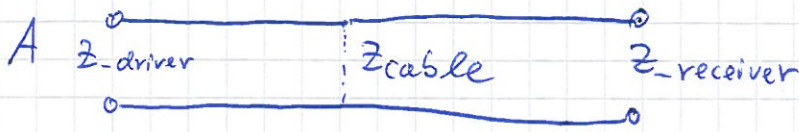
$\epsilon = \text{dielectricity}$
 $\epsilon_r = \text{dielectric constant}$
 $\epsilon = \epsilon_0 \epsilon_r$

$$\tilde{L} = \frac{\Delta L}{\Delta l} = \frac{\mu}{2\pi} \ln(b/a) = \mu_r \cdot 0.2 \mu\text{H/m} \cdot \ln(b/a)$$

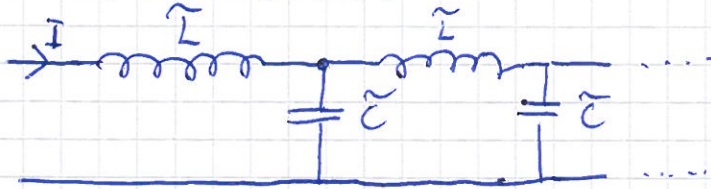
$\mu = \mu_0 \mu_r$ $\mu_r \approx 1$ for PE
 permeability

Signal transmission in wave guide

transmission from A → B



wire representation:



Induction:

$$\Delta V = -\tilde{L} \cdot \Delta z \cdot \frac{\partial I}{\partial t}(z, t) \quad \left(U_{ind} = -L \frac{\partial I}{\partial t} \right)$$

Condensator:

$$\Delta I = -\tilde{C} \cdot \Delta z \cdot \frac{\partial V}{\partial t}(z, t) \quad \left(Q = C \cdot V \quad I = \frac{\partial Q}{\partial t} \right)$$

$$\frac{\partial}{\partial z} \Big| \quad \frac{\partial V}{\partial z} = -\tilde{L} \frac{\partial I}{\partial t} \quad \Rightarrow \quad \frac{\partial^2 V}{\partial z^2} = -\tilde{L} \frac{\partial^2 I}{\partial z \partial t}$$

$$\frac{\partial}{\partial t} \Big| \quad \frac{\partial I}{\partial z} = -\tilde{C} \frac{\partial V}{\partial t} \quad \Rightarrow \quad \frac{\partial^2 I}{\partial z \partial t} = -\tilde{C} \frac{\partial^2 V}{\partial t^2}$$

⇒ combination:

$$\frac{\partial^2 V}{\partial z^2} = \tilde{L} \tilde{C} \frac{\partial^2 V}{\partial t^2} \quad (\text{wave equation})$$

$$\frac{1}{v^2} \Rightarrow \text{group velocity } v = \frac{1}{\sqrt{\tilde{L} \tilde{C}}}$$

$$\Rightarrow \text{plugging in numbers: } v = \frac{1}{\sqrt{\frac{2\pi \cdot \epsilon_r \cdot \epsilon_0}{\ln(b/a)} \cdot \frac{\mu_0 \mu_r}{2\pi} \ln(b/a)}} = \frac{1}{\sqrt{\epsilon_r \mu_r \epsilon_0 \mu_0}}$$

$$\text{speed of light: } c = \frac{1}{\sqrt{\epsilon_0 \mu_0}} \Rightarrow v = \frac{c}{\sqrt{\epsilon_r \mu_r}} \approx \frac{c}{\sqrt{23}} = 0.66 c \approx 20 \text{ cm/ns}$$

(5)

Solution of wave equation:

⇒ sine wave (cosine)

$$U = U_0 e^{i(kz - \omega t)}$$

$$\frac{\partial U}{\partial t} = -i\omega U_0 e^{i(kz - \omega t)}$$

$$\frac{\partial U}{\partial t} = -i\omega U_0$$

$$\bar{I} = I_0 e^{i(kz - \omega t)}$$

$$\frac{\partial \bar{I}}{\partial t} = i k I_0 e^{i(kz - \omega t)}$$

$$\frac{\partial \bar{I}}{\partial t} = i k \bar{I}$$

from previous calculation (capacity)

$$\frac{\partial \bar{I}}{\partial z} = -\tilde{C} \frac{\partial U}{\partial t}$$

$$i k \bar{I} = +\tilde{C} i \omega U$$

Definition of Impedance

$$\text{impedance: } Z = \frac{U}{\bar{I}} = \frac{k}{\omega \tilde{C}}$$

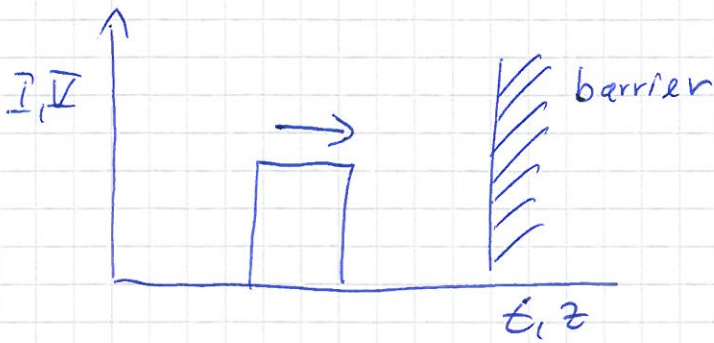
$$\text{using } v = \frac{\omega}{k} = \frac{1}{\sqrt{\tilde{L}\tilde{C}}}$$

$$\Rightarrow Z = \sqrt{\frac{\tilde{L}}{\tilde{C}}} = \sqrt{\frac{\mu_r \mu_0 \ln(b/a)}{2\pi \cdot 2\pi \epsilon_0 \epsilon_r / \ln(b/a)}} = \frac{\ln(b/a)}{2\pi} \sqrt{\frac{\mu_r \mu_0}{\epsilon_r \epsilon_0}} = 50-75 \Omega$$

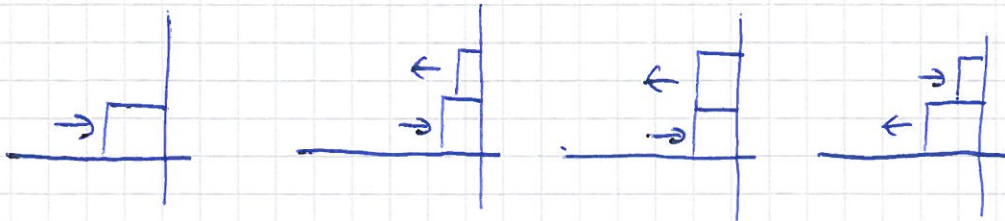
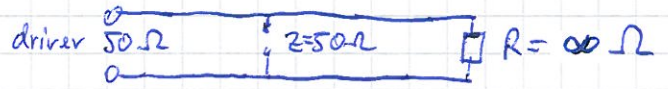
Comment: 1000 Ω impossibleNote: $Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 \Omega$ (vacuum impedance)

Comment: real losses due to resistance of cables are negligible

Reflection and Termination



Schematics!



Signal is twice as big

• Solution:

⇒ correct termination



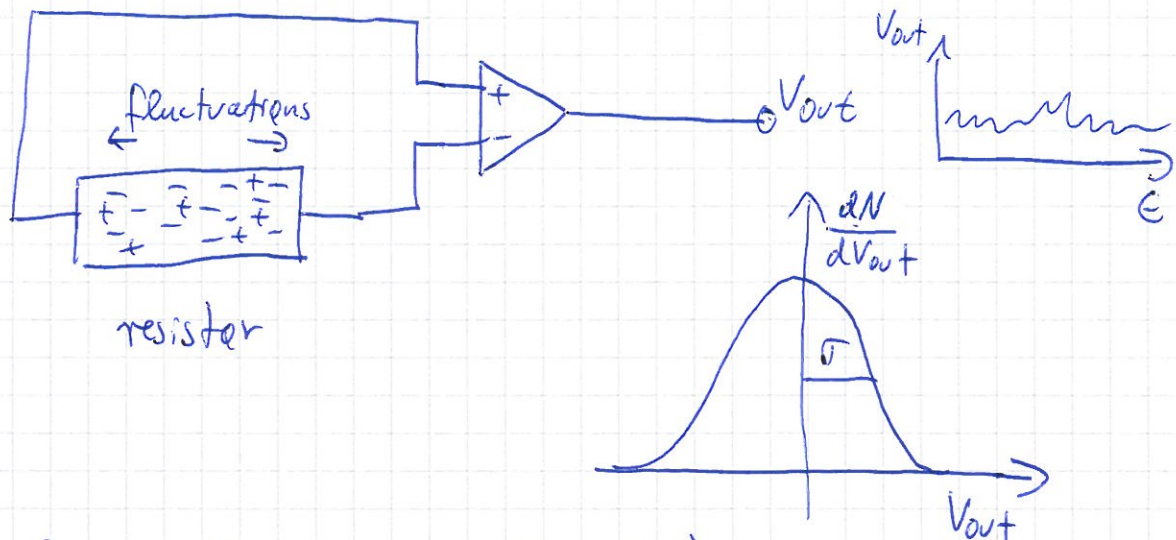
• Oscilloscope has two different input settings:

- 50Ω
- $1M\Omega$

Noise

(7)

- Johnson Noise (Nyquist) \Rightarrow thermal noise



Width of noise distribution (Gaussian) given by:

$$\sigma = V_{RMS} = \sqrt{4k_B T \cdot R \cdot \Delta f}$$

k_B = Boltzmann constant = $1.38 \cdot 10^{-23} \text{ J/K}$

T = temperature

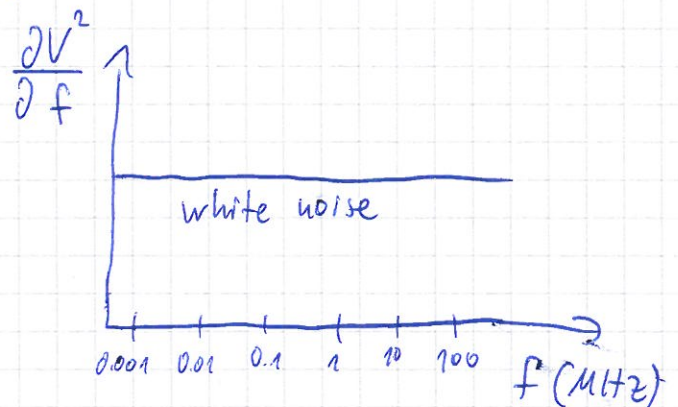
Δf = bandwidth (frequency cutoff)

Example:

$$R = 10 \text{ k}\Omega$$

$$T = 300 \text{ K}$$

$$\Delta f = 100 \text{ MHz}$$



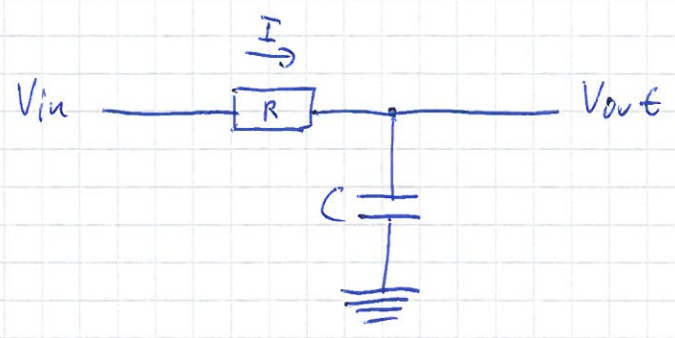
$$\Rightarrow V_{RMS}^{noise} = 0.13 \text{ mV}$$

Noise dependence:

- temperature
- resistance
- bandwidth

Rising Times and Bandwidth

Low Pass Filter



$$V_R = R \cdot I$$

$$V_{in} = V_R + V_{out}$$

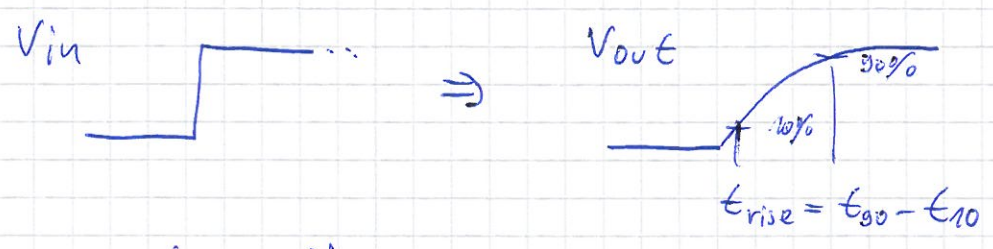
$$I = \frac{dQ}{dt} = C \frac{dV_{out}}{dt}$$

$$\Rightarrow V_{in} = R \cdot C \frac{dV_{out}}{dt} + V_{out}$$

differential equation
solved by separating variables

$$\Leftrightarrow \frac{dt}{RC} = \frac{dV_{out}}{V_{in} - V_{out}}$$

Solution: $V_{out} = V_{in} (1 - e^{-t/RC})$



$$t = -\ln\left(1 - \frac{V(t)}{V_{in}}\right) \cdot RC$$

$$t_{90} = -\ln(0.1) \cdot RC$$

$$t_{10} = -\ln(0.9) \cdot RC$$

$$t_{90} - t_{10} = \ln(9) \cdot RC = 2.2 \cdot RC$$

Rising time given by time constant $\tau = RC$

Low Pass Filter (cont'd)

A low pass filter is an integrator (RC-circuit)



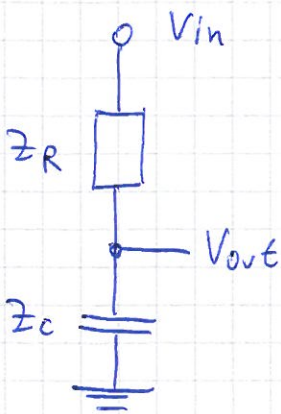
$$V_{in} = RC \frac{dV_{out}}{dt} + V_{out} \quad \left(\text{using } I = \frac{dQ}{dt} = C \frac{dV_{out}}{dt} \right)$$

for $V_{out} \ll V_{in}$ (short time pulse)

$$\Rightarrow V_{in} = RC \frac{dV_{out}}{dt} \Leftrightarrow \boxed{V_{out} = \int dt \frac{V_{in}}{RC}} \quad \text{integrieren!}$$

Solution for arbitrary frequencies

voltage divider:

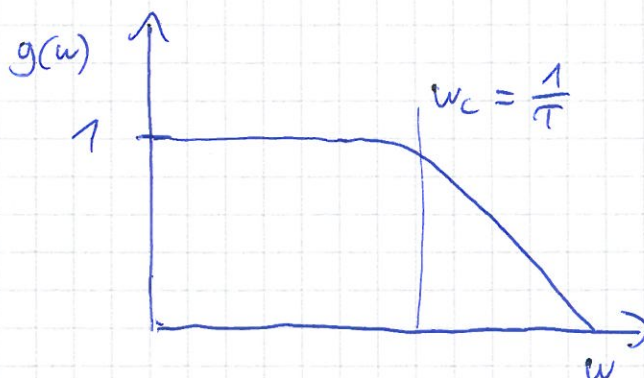


$$V_{out} = V_{in} \cdot \frac{Z_c}{Z_R + Z_c}$$

$$\begin{aligned} Z_R &= R \\ Z_c &= \frac{1}{i\omega C} \\ \tau &= RC \end{aligned}$$

$$\Rightarrow \frac{V_{out}}{V_{in}} = \frac{1}{1+i\omega RC} = \frac{1}{1+i\omega\tau}$$

$$\text{ratio } g(\omega) = \left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1+\omega^2\tau^2}}$$

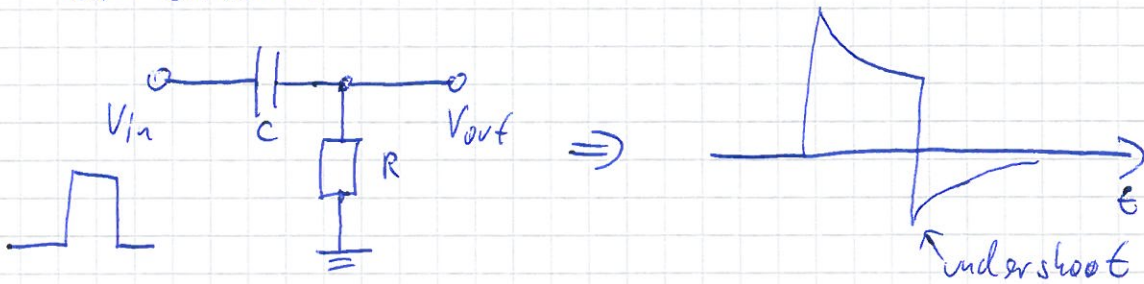


$$\begin{aligned} \omega\tau \ll 1 &\Rightarrow g(\omega) = 1 \\ \omega\tau \gg 1 &\Rightarrow g(\omega) = \frac{1}{\omega\tau} \end{aligned}$$

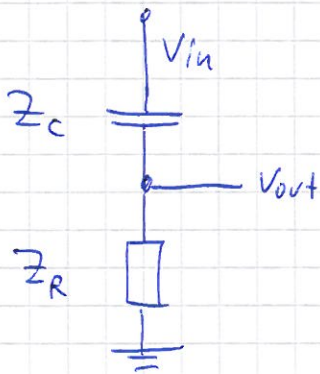
High Pass Filter (differentiator)

(10)

CR circuit:

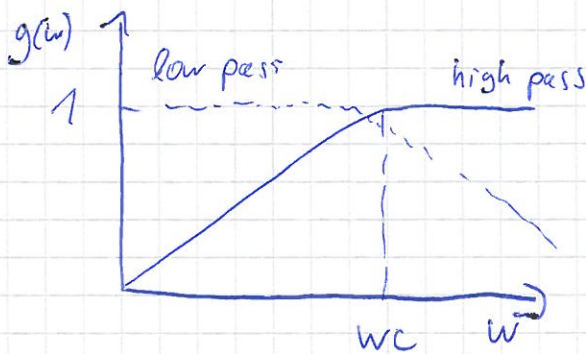


drawn as voltage divider:



$$V_{out} = V_{in} \frac{Z_R}{Z_R + Z_C} = \frac{R}{R + \frac{1}{i\omega C}}$$

$$g(\omega) = \left| \frac{V_{out}}{V_{in}} \right| = \frac{\omega RC}{\sqrt{1 + \omega^2 R^2 C^2}} = \frac{\omega T}{\sqrt{1 + \omega^2 T^2}}$$



o By combining low pass and high pass filters only small frequency range is selected \Rightarrow suppresses noise!

o decibel:

$$E \propto g^2(\omega) \quad L = 10 \log_{10} \left(\frac{g(\omega)^2}{g(0)^2} \right) = 20 \log_{10} \left(\frac{g(\omega)}{g(0)} \right)$$

$$\frac{g(\omega)}{g(0)} = \frac{1}{\sqrt{2}} \quad \Rightarrow \quad L = 20 \cdot \log_{10} \frac{1}{\sqrt{2}} = -3 \text{ dB}$$

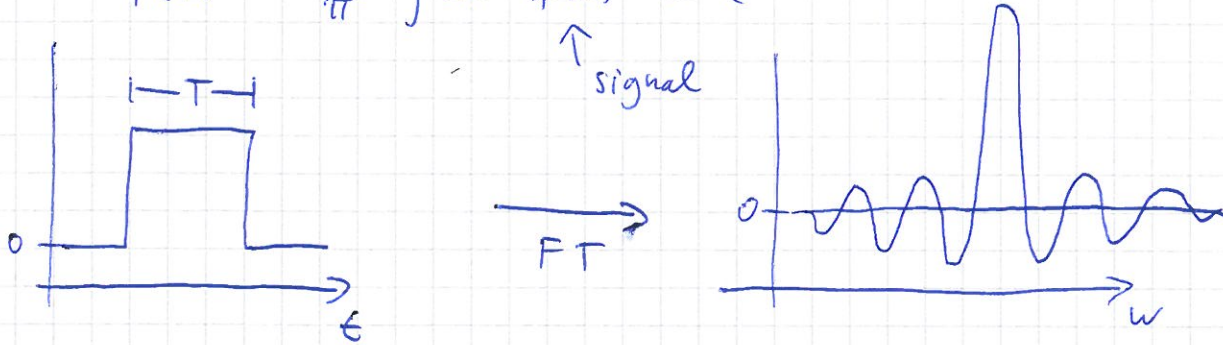
Pulse Shaping

• combination of CR-CR circuits shapes pulses:

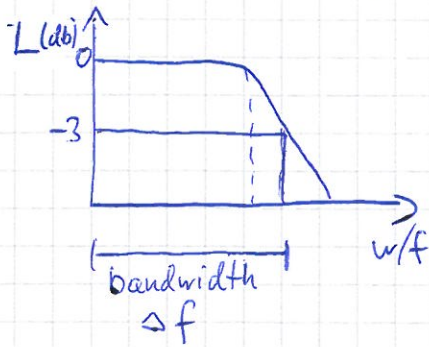


• general case → Fourier Transformation:

$$f(\omega) = \frac{1}{\pi} \int d\epsilon \uparrow \text{signal } f(\epsilon) \cos(\omega\epsilon)$$

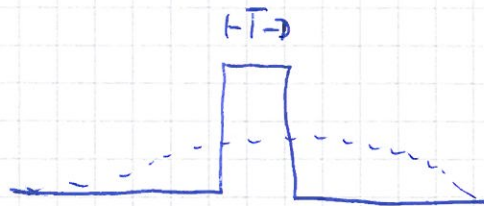


• example: low pass filter:



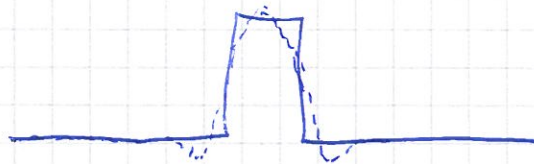
-3db defines bandwidth Δf

A: $\Delta f = \frac{0.1}{T}$

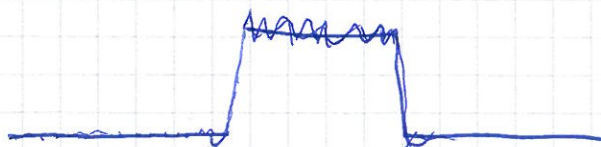


small bandwidth

B: $\Delta f = \frac{1}{T}$



C: $\Delta f = \frac{10}{T}$

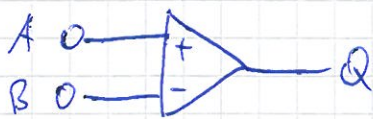


high bandwidth

Amplification

(12)

o operational amplifier \rightarrow ideal amplifier



$$I_Q = +\infty \quad \text{if } V_A > V_B$$

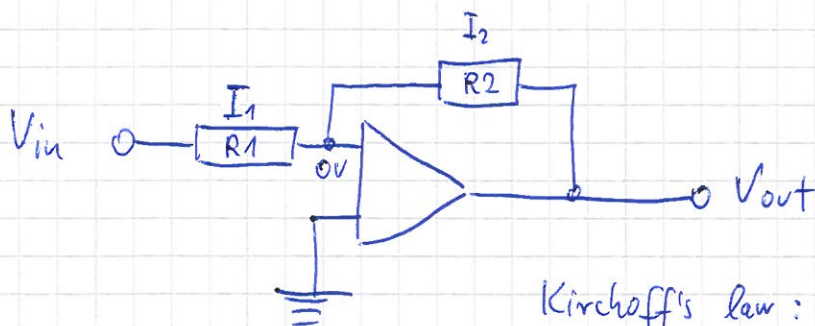
$$I_Q = -\infty \quad \text{if } V_A < V_B$$

$$I_Q = 0 \quad \text{if } V_A = V_B$$

low output impedance: $Z_Q = 0$

high input impedance: $Z_A = Z_B = \infty$

Example: voltage amplifier



Kirchoff's law: $I_1 = I_2$

$$I = \frac{V_{in}}{R_1} = -\frac{V_{out}}{R_2} \Rightarrow V_{out} = -V_{in} \frac{R_2}{R_1}$$

for $\frac{R_2}{R_1} > 1$ amplification

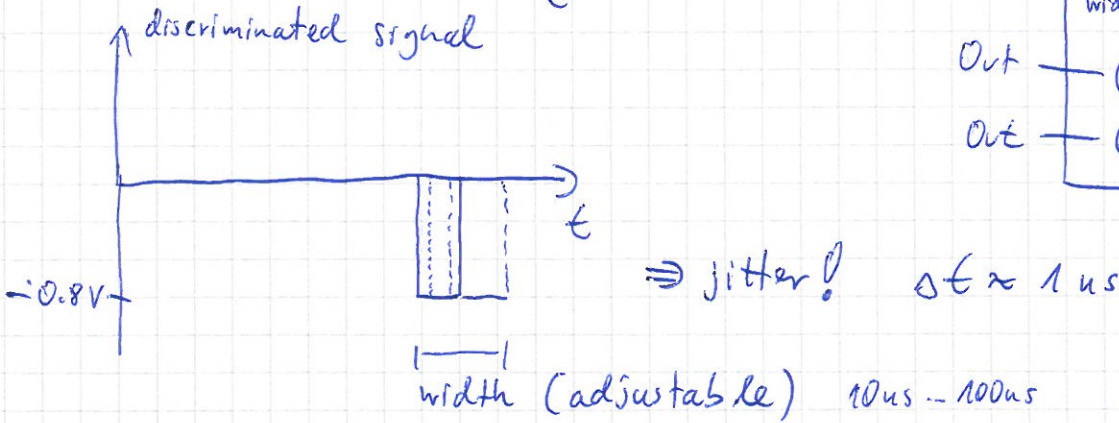
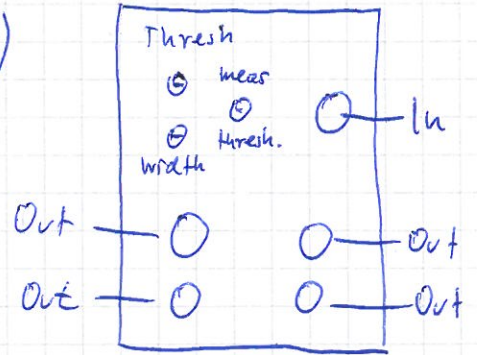
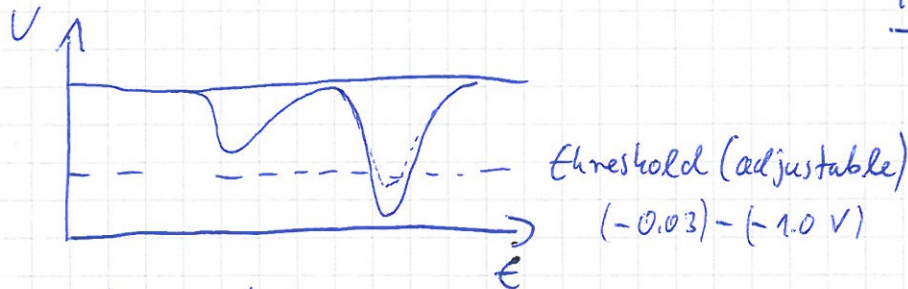
Note: also (thermal) noise is amplified

\rightarrow limitation $\frac{R_2}{R_1} < 1000$

Discriminators

o Constant Threshold

Hardware:



different operational modes:

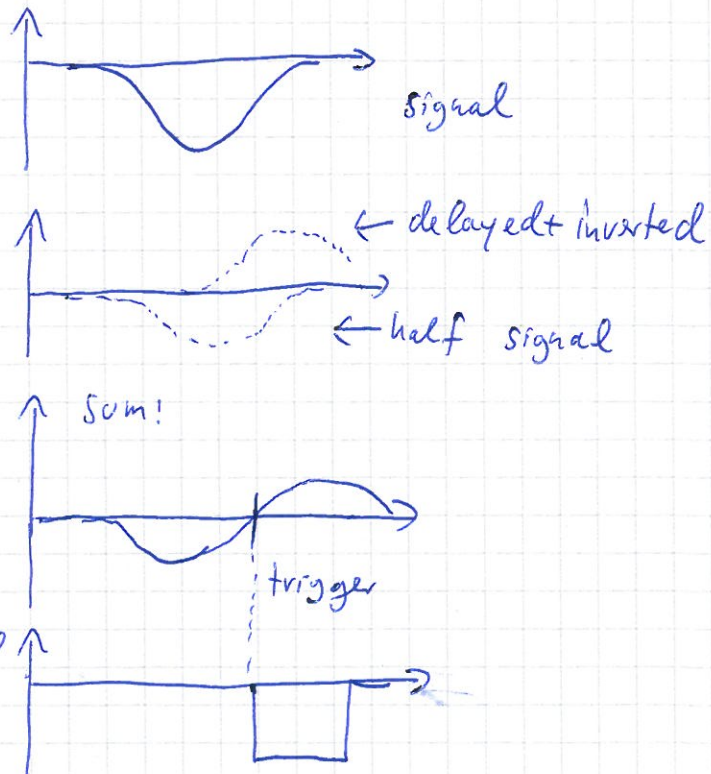
- updating (signal ends wrt. to last falling edge)
- non-updating (signal ends wrt rising edge)

o Constant Fraction

→ for good timing

- split signal
- invert and delay
- sum
- zero-crossing defines time!

Method:



note: delay should correspond to signal width

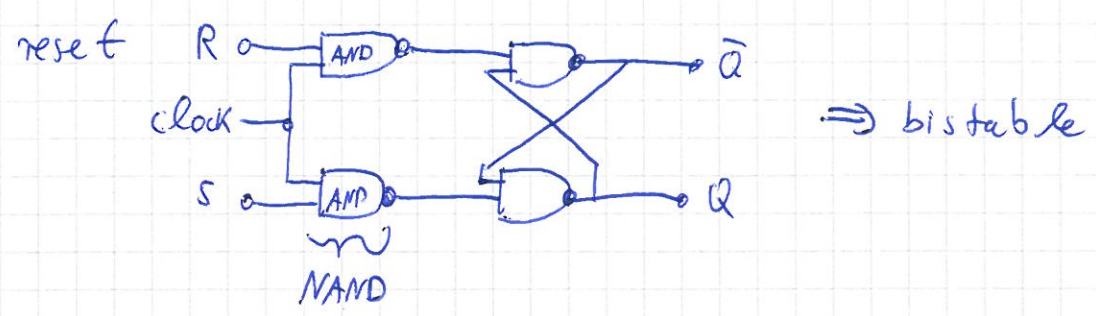
- trigger independent of signal height! $V_{max}/V_{min} \approx 1000$
- ⇒ reduced jitter $\Delta t \approx 20ps$

Digital Electronics

- o logic states "low" and "high"
 - different signal standards:
 - e.g. NM fast "low" = 0V "high" \approx -0.8V !
- o applications:
 - processors
 - networks
 - memories
- o Signal transmission:
 - electronically \approx 1 Gbit/s per channel
- o Components
 - converter
 - ADC (analog to digital)
 - DAC (digital to analog)
 - e.g. ADC, TDC, TAC, ...
 - Memories (buffer)
 - Logical operations
 - coincidences
 - scaler (counter)
 - adder
- FPGAs (field programmable gate arrays)

Buffer (flip flop)

smallest element of any memory



Logic table

R	S	Q	\bar{Q}
0	0	\bar{Q}	\bar{Q}
1	0	0	1
0	1	1	0
1	1	1	1

} $Q = \bar{Q}$

forbidden / undefined)

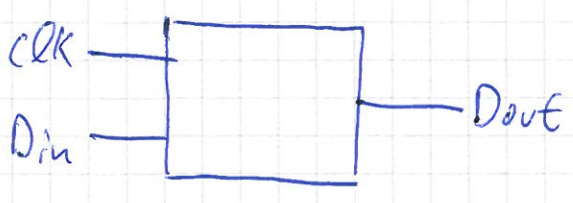
=> RS flip flop

(JK flip flop)

↳ triggers on falling clock edge!

D - flip flop

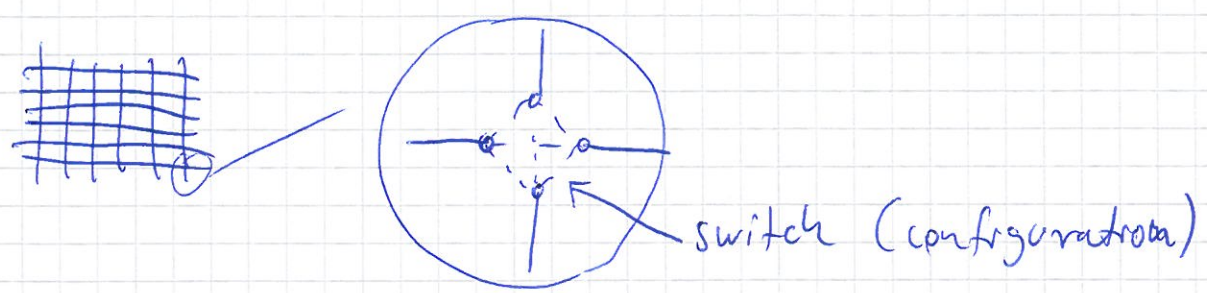
-> used in FPGA



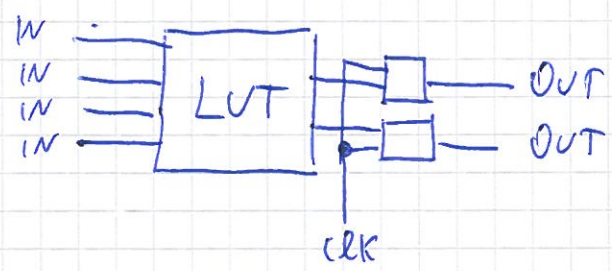
=> Dout takes state of Din at rising clock.

FPGA (field programmable gate array)

1. field of wires connection thousands of elements:



2. elements (logical cells)



LUT = lookup table

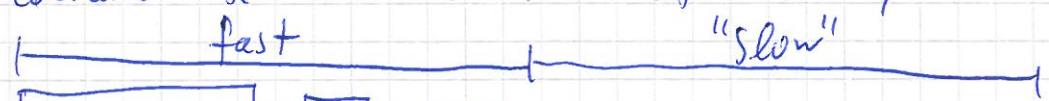
Address	Value
0 0 0 0	0 0
0 0 0 1	0 1
0 0 1 0	0 0
0 0 1 1	1 0
0 1 0 0	0 1
0 1 0 1	1 0
0 1 1 0	1 0
0 1 1 1	1 1
!	!

a lookup table can be configured as:

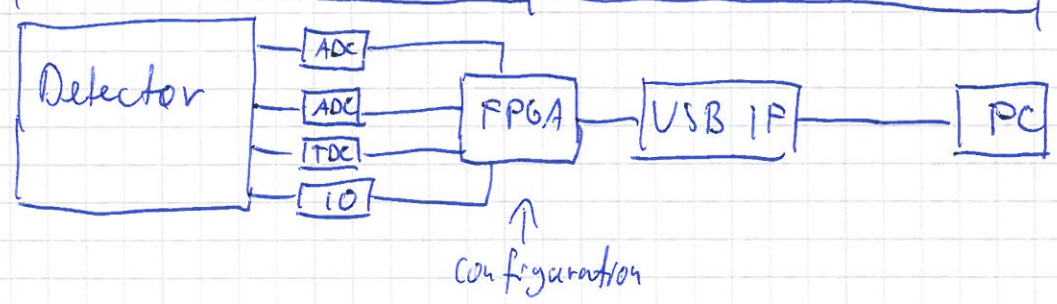
- adder
- coincidence
- inverter
- etc.

3. Memories

FPGAs contain several KB - MB of memory



4. Usage:



Analog to Digital Converters (ADC)

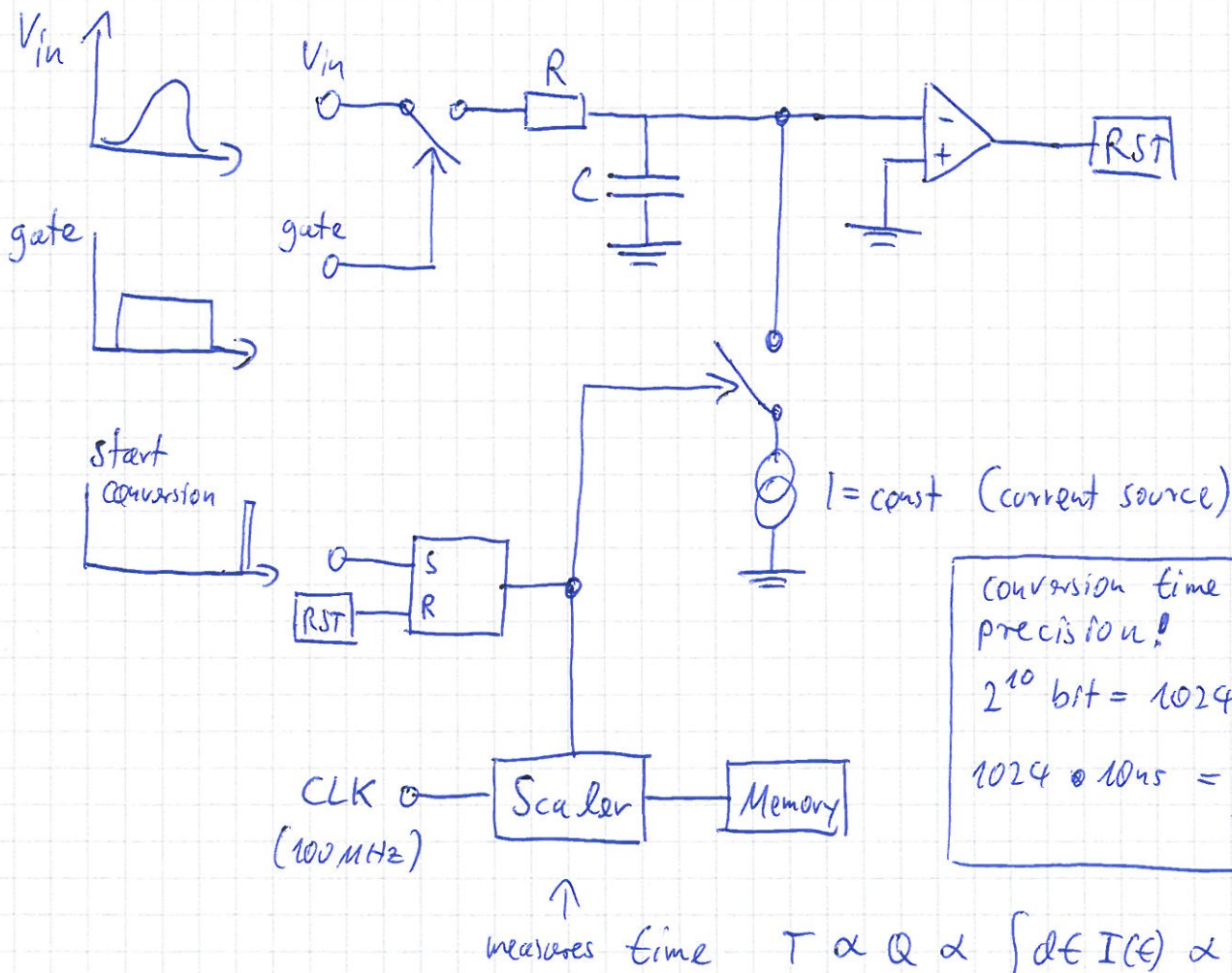
o Different types:

- voltage (peak voltage)
- charge
- fast ADCs with sampling (e.g. Flash ADC)

o Wilkinson ADC

method/principle:

- charge condenser (capacity) when gate open
- convert charge into a time signal by discharging capacity
- measure time for discharge with a scaler \Rightarrow conversion time



conversion time determines precision!

$2^{10} \text{ bit} = 1024 \quad 100 \text{ MHz} \approx 10 \text{ ns}$

$1024 \cdot 10 \text{ ns} = \underline{\underline{10 \mu\text{s}}}$

- o resistor can be replaced by diode to measure peak of signal!
- o "old" TDC has similar design

Fast ADCs

(18)

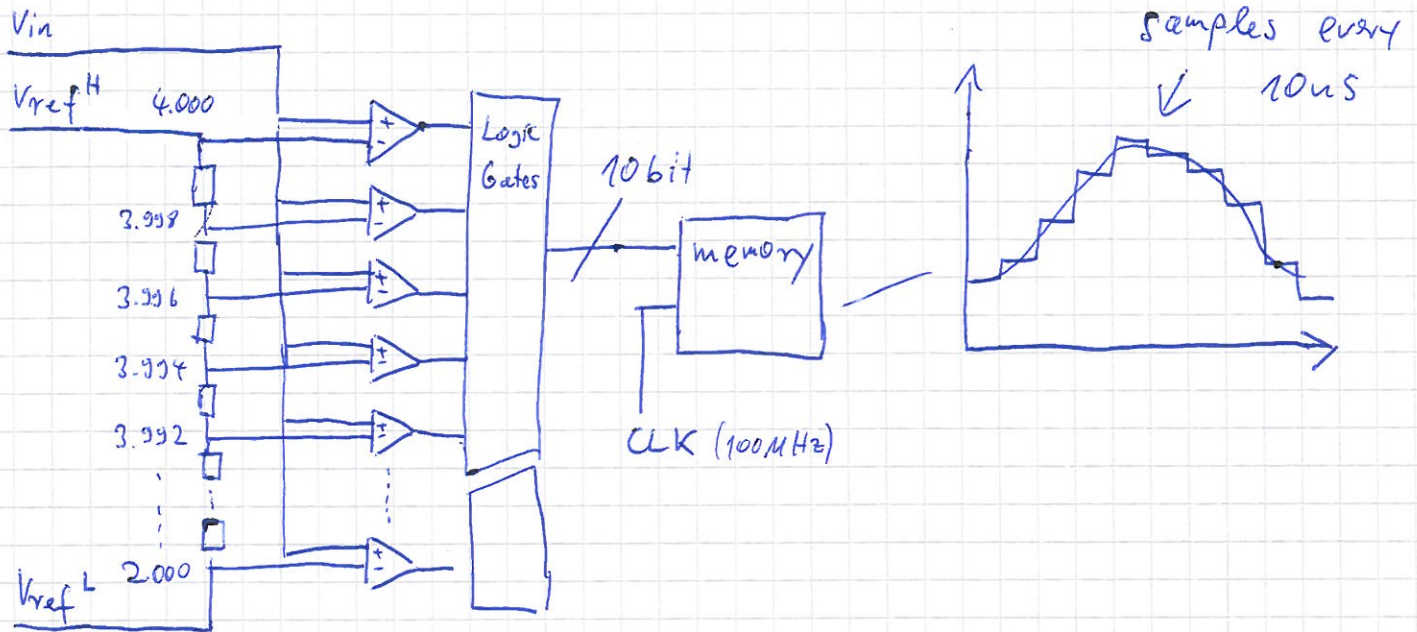
Flash ADC (network / resistor chain)

• 2^n comparators and 2^n precision resistors

10 bit \Rightarrow 1024

12 bit \Rightarrow 4096

16 bit \Rightarrow 65536

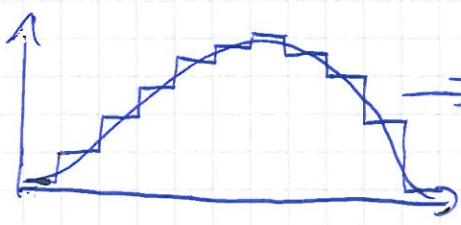


• difficult to build FAOC with more than 10-12 bit

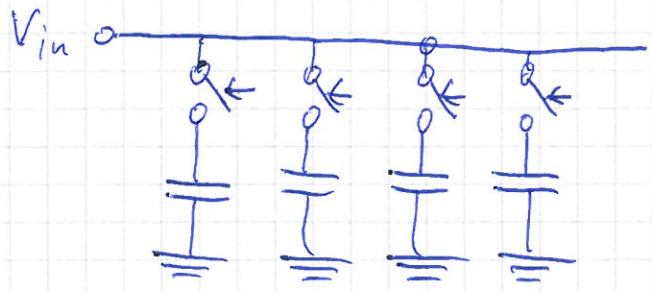
• nowadays:

\Rightarrow capacity switched ADC

Capacity Switched ADC (fast ADC)



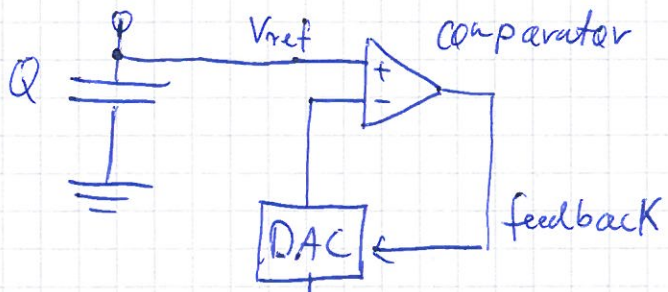
store samples in quickly charged capacitors



100 MHz clock (round robin)

Memory of analog charges

Digitisation



actually several DACs and comparators are used

DAC = digital to analog converter

10-16 bit

Sample @ 100 MHz

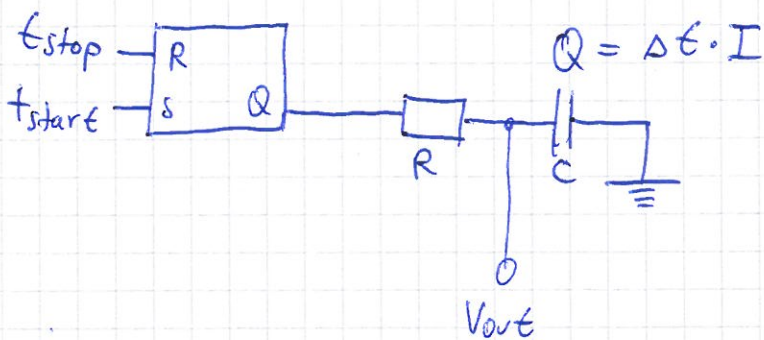
Time to Analog Converter (TAC)

(20)

o Method:

- t_{start} and t_{stop} used to charge capacity:

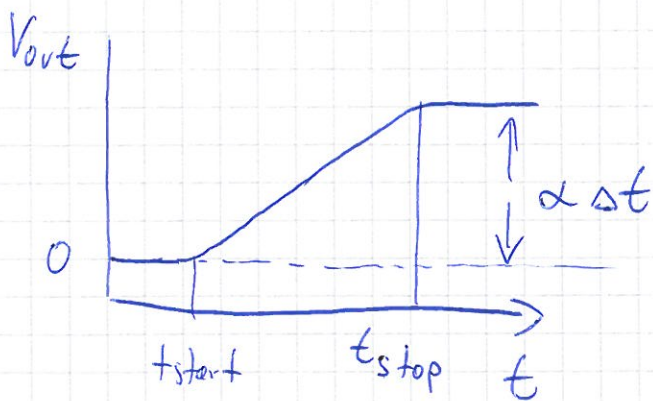
$$Q \propto (t_{start} - t_{stop})$$



for $\Delta t \ll R \cdot C$
(linearisation)

o Output signal V_{out} is proportional to time difference.

⇒ input to fast ADC

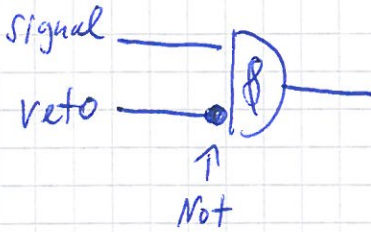


⇒ used to measure very short times. $\approx 20 \text{ ps}$



Trigger

o Different NIM logic components available to implement coincidences, delay, discriminators etc.

coincidences



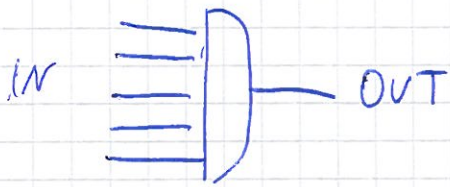
check timing (synchronisation) of signals

→ jitter

→ delays

fan in:

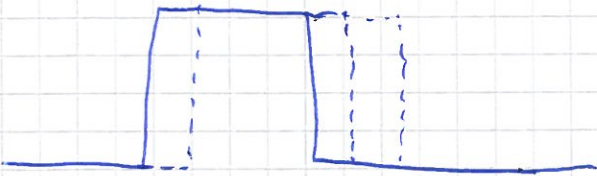


coincidence or analog sum

fan out:



delay triggers:



- used to delay signals $\mu s - s$
- used to generate long signals $\mu s - s$
- can be configured as buffer (reset)

Signal Standards (in HEP)

Standard	$V_{\text{driver}} \text{ (V)}$		$I \text{ (mA)}$		$Z_{\text{in}} \text{ (}\Omega\text{)}$	
	low	high	low	high		
NIM fast	[0]	[-0.7, -0.9]	0	[-14, -18]*	50	fast/negative
NIM slow	[-2, +1]	[+4, +12]	~ 0	[+4, +12]	> 1K	slow
ECL	-0.9	-1.75	-78	-36	50 (100)	fast/negative/ high power
TTL 5	[0, 0.8]	5	~ 1		> 1K	industry
TTL 2.3	[0, 0.8]	3.3	~ 1		> 1K	standard

